

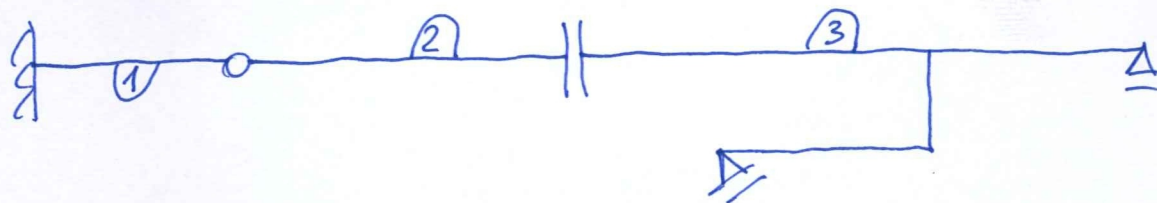
1 Spr. GN i SW

* war ilościowy

$$n = e - 3t$$

$$n = 9 - 3 \cdot 3 = 0$$

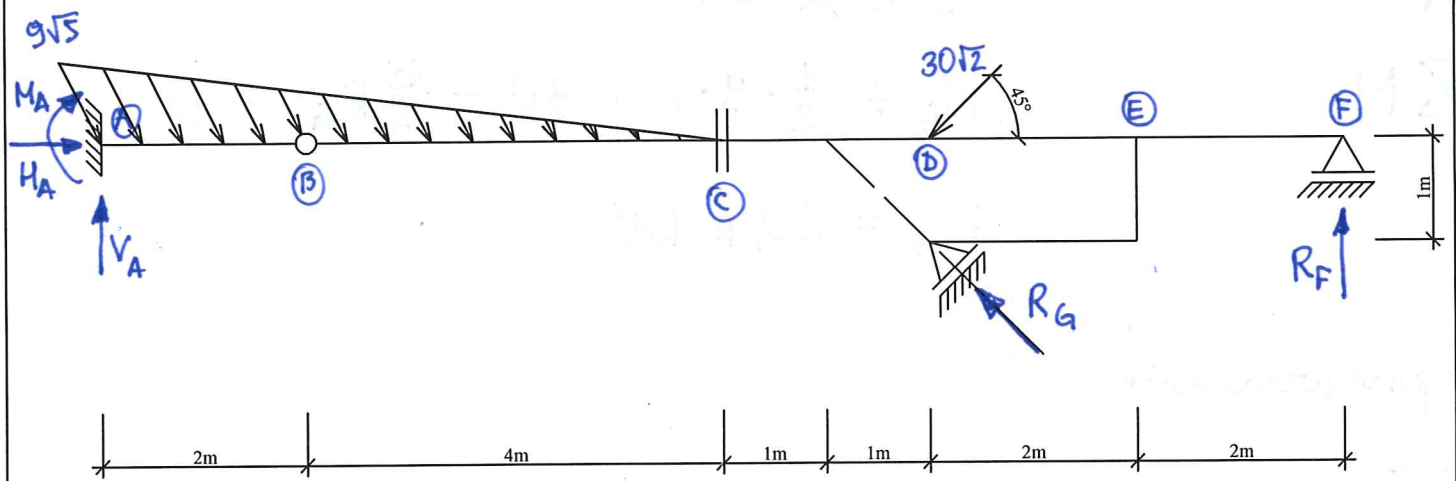
* war jakościowy



Z tw. o 2 tarasach ① GN.

Z tw. o 3 tarasach ② ③ GN

Układ jest geometrycznie niezmienny i statycznie wyznaczalny.



2 Reakcje

War. konstankyjung

$$\sum y_L^c = 0$$

$$-V_A + \frac{1}{2} \cdot 6 \cdot 9\sqrt{5} \cdot \frac{2}{\sqrt{5}} = 0$$

$$V_A = 54 \text{ kN}$$

War. konstankyjung

$$\sum M_B(l) = 0$$

$$M_A + 2V_A - 2 \cdot 12 \cdot 1 - \frac{1}{2} \cdot 6 \cdot 2 \cdot \frac{4}{3} = 0$$

$$M_A = -76 \text{ kNm}$$

$$\sum M_F = 0$$

$$M_A + 12V_A - \frac{1}{2} \cdot 6 \cdot 18 \cdot 10 - 4 \cdot 30 + 5 \cdot \frac{\sqrt{2}}{2} R_G = 0$$

$$\frac{5\sqrt{2}}{2} R_G = 88$$

$$R_G = 24,89 \text{ kN}$$

$$R_{Gx} = R_{Gy} = 17,6 \text{ kN}$$

War konstankyjung

$$\sum y_P^c = 0$$

$$30 - R_{Gy} - R_F = 0 \Rightarrow R_F = 12,4 \text{ kN}$$

$$\sum X = 0$$

$$M_A + \frac{1}{2} \cdot 9 \cdot 6 - 30 - \frac{\sqrt{2}}{2} R_G = 0$$

$$M_A = 20,6 \text{ kN}$$

Sperrachse

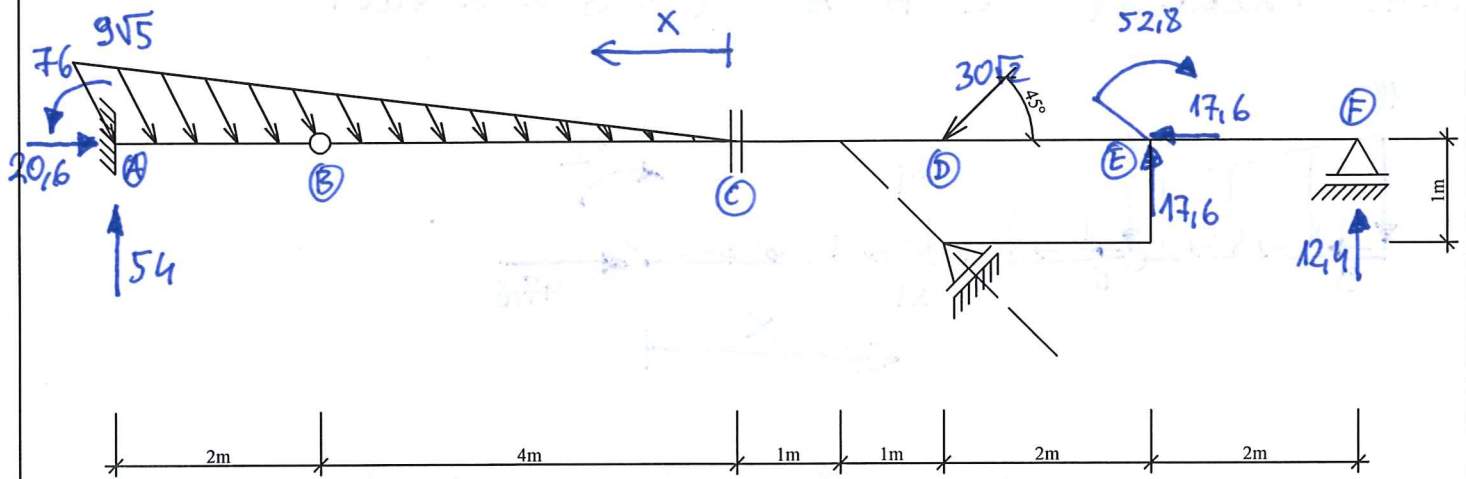
$$\sum M_E = 0$$

$$10 V_A + M_A - \frac{1}{2} \cdot 18 \cdot 6 \cdot 8 - 2 \cdot 30 + 3 \cdot R_{Gy} - 2 R_F =$$

$$= 10 \cdot 59 - 76 - 432 - 60 + 3 \cdot 17,6 - 2 \cdot 12,4 =$$

$$= 592,8 - 592,8 = 0 \quad \leftarrow \text{ok!}$$

SCHEMAT OBLICZENIOWY



3. Siły przekrojowe

3.1. Przekrój F-E

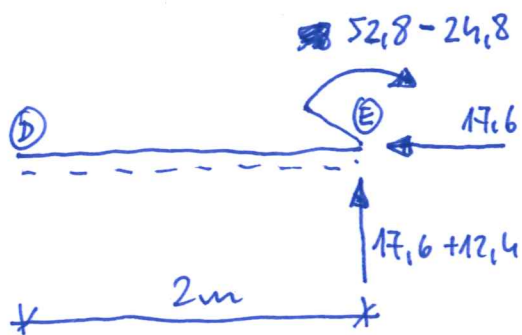
$$M_{FE} = 0, \quad M_{EF} = 2 \cdot 12,4 = 24,8 \text{ kNm}$$

$$T_{FE} = T_{EF} = -12,4 \text{ kN}$$

$$N_{FE} = N_{EF} = 0$$



3.2. Przekrój E-D



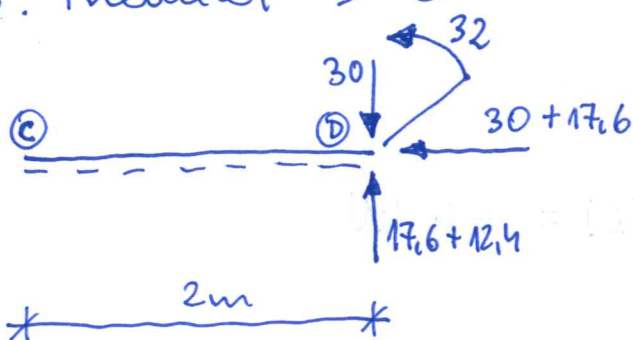
$$M_{ED} = -52,8 + 24,8 = -28 \text{ kNm}$$

$$M_{DE} = -28 + 2(17,6 + 12,4) = 32 \text{ kNm}$$

$$T_{DE} = T_{ED} = -(17,6 + 12,4) = -30 \text{ kN}$$

$$N_{DE} = N_{ED} = -17,6 \text{ kN}$$

3.3. Przekrój D-C



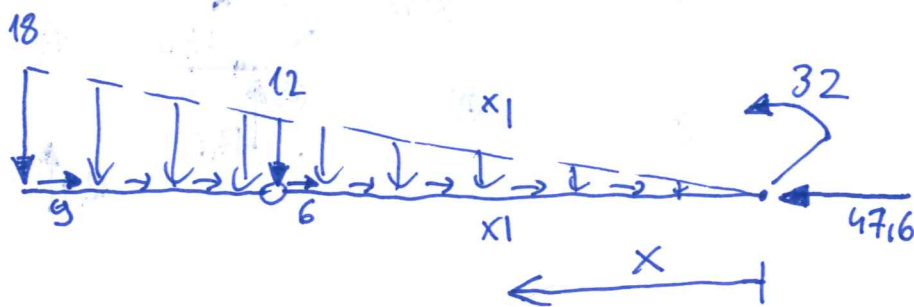
$$M_{DC} = 32 \text{ kNm}$$

$$M_{CD} = 32 - 2 \cdot 30 + 2 \cdot (17,6 + 12,4) = 32 \text{ kNm}$$

$$T_{DC} = T_{CD} = 30 - 17,6 - 12,4 = 0$$

$$N_{DC} = N_{CD} = -30 - 17,6 = -47,6 \text{ kN}$$

3.4. Przekrój C-B-A ($0 \leq x \leq 6\text{m}$)



$$M(x) = 32 - \frac{1}{2} \cdot x \cdot \frac{18}{6} x \cdot \frac{x}{3} = -\frac{1}{2} x^3 + 32$$

$$T(x) = +\frac{1}{2} \cdot x \cdot \frac{18}{6} x = 1,5 x^2$$

$$N(x) = -47,6 + \frac{1}{2} \frac{9}{6} x \cdot x = 0,75 x^2 - 47,6$$

$$T(x_0) = 0 \Leftrightarrow 1,5 x^2 = 0 \Rightarrow x_0 = 0$$

Na przekroju nie występuje ekstremum momentu

$$M(0) = 32 \text{ kNm}$$

$$M(2) = 28 \text{ kNm}$$

$$M(4) = 0 \quad - \text{przebieg}$$

$$M(6) = -76 \text{ kNm}$$

$$T(0) = 0$$

$$T(2) = 6 \text{ kN}$$

$$T(4) = 24 \text{ kN}$$

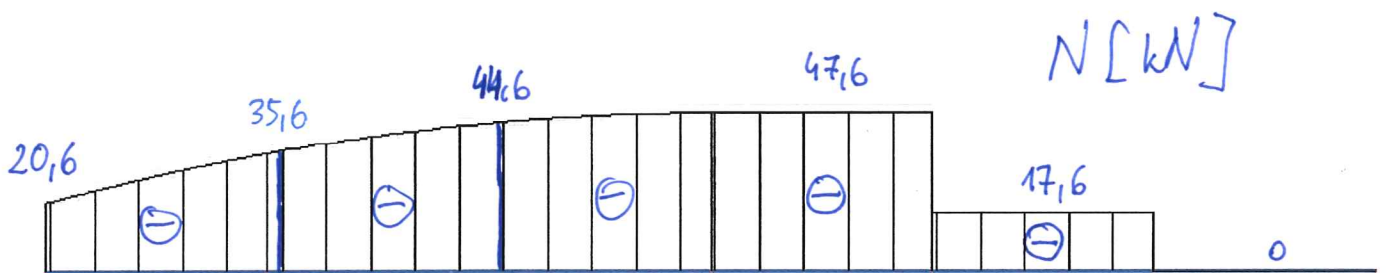
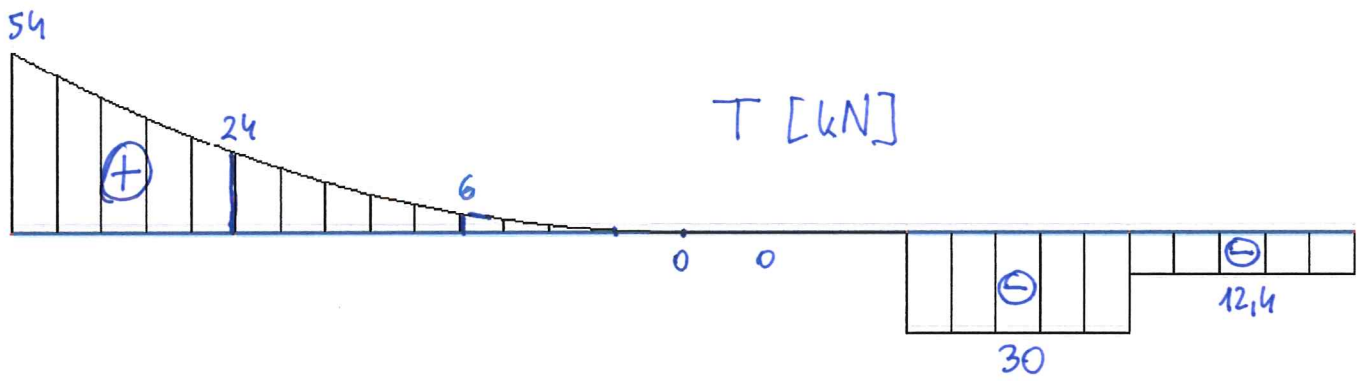
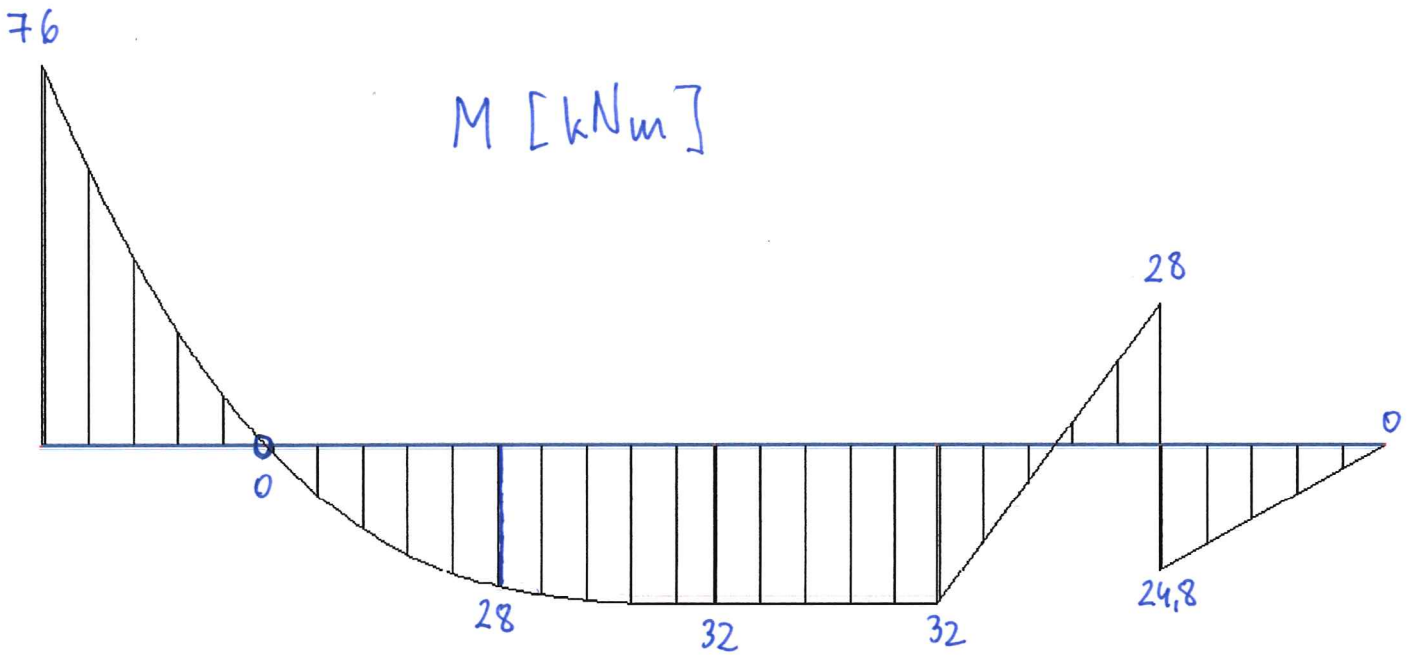
$$T(6) = 54 \text{ kN}$$

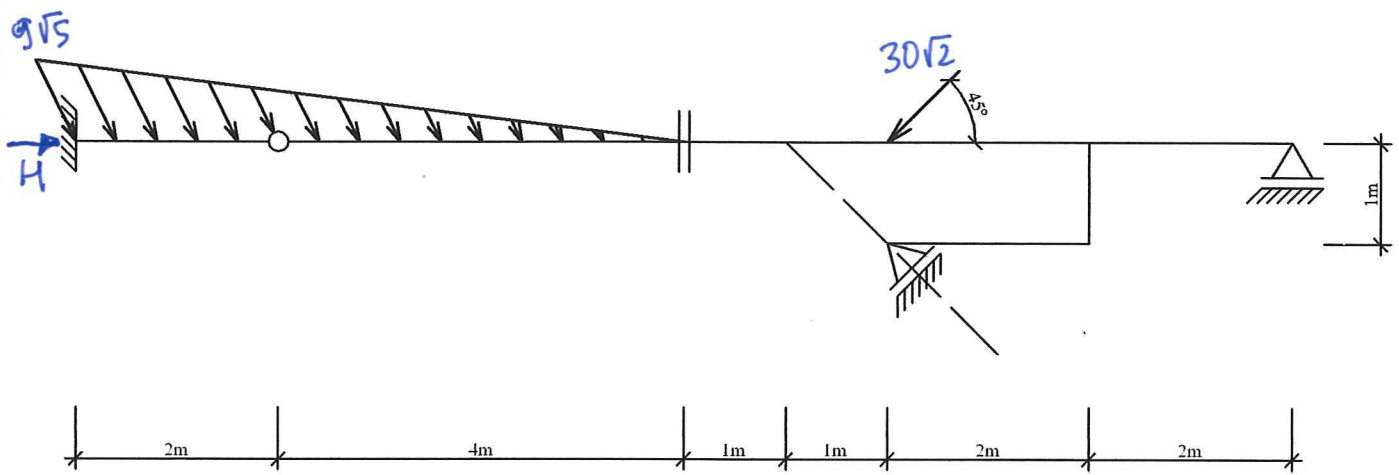
$$N(0) = -47,6 \text{ kN}$$

$$N(6) = 6,4 \text{ kN}$$

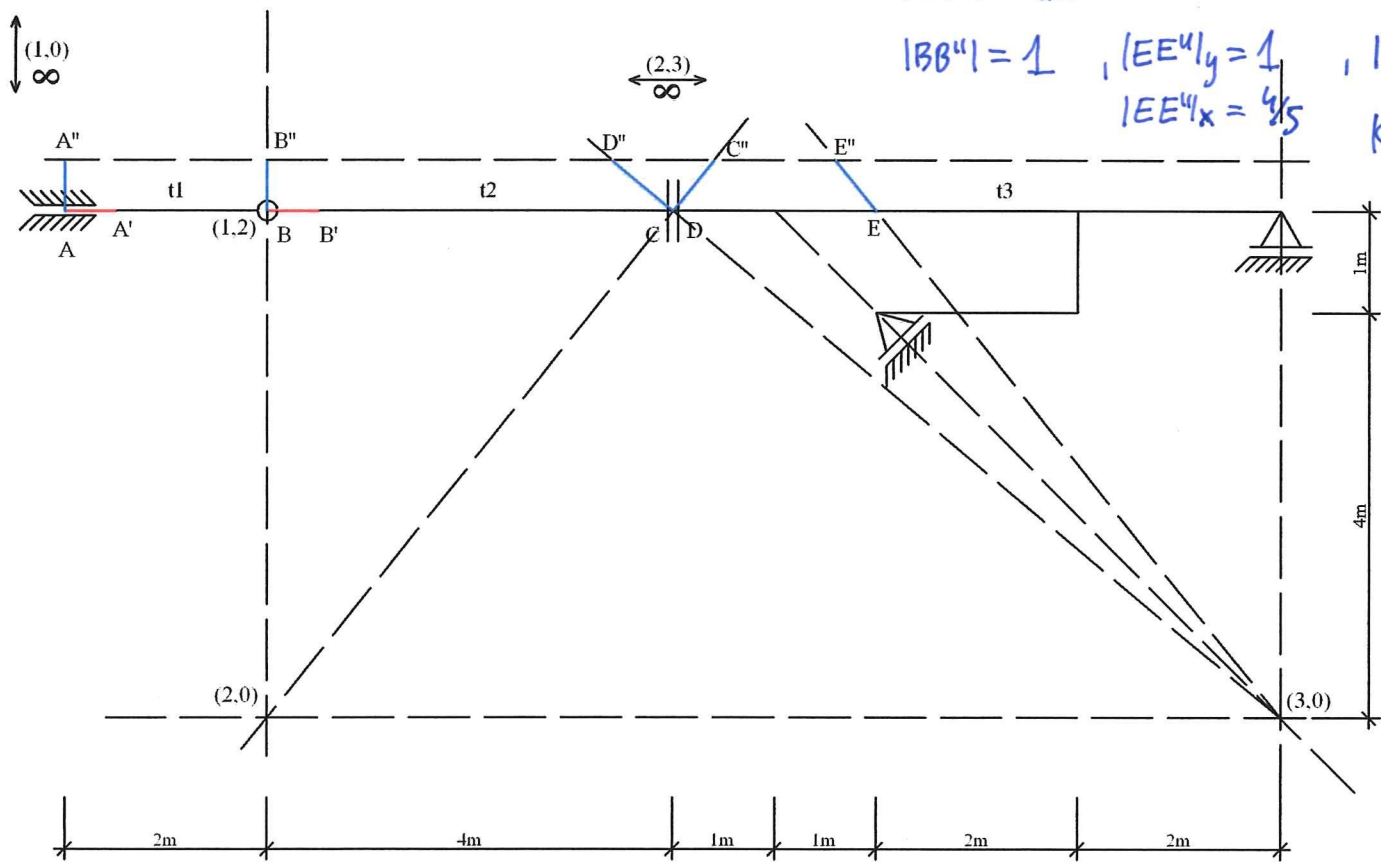
$$N(2) = -44,6 \text{ kN}$$

$$N(4) = -35,6 \text{ kN}$$





Medanimum "H"



$|AA''| = 1$ - mediane

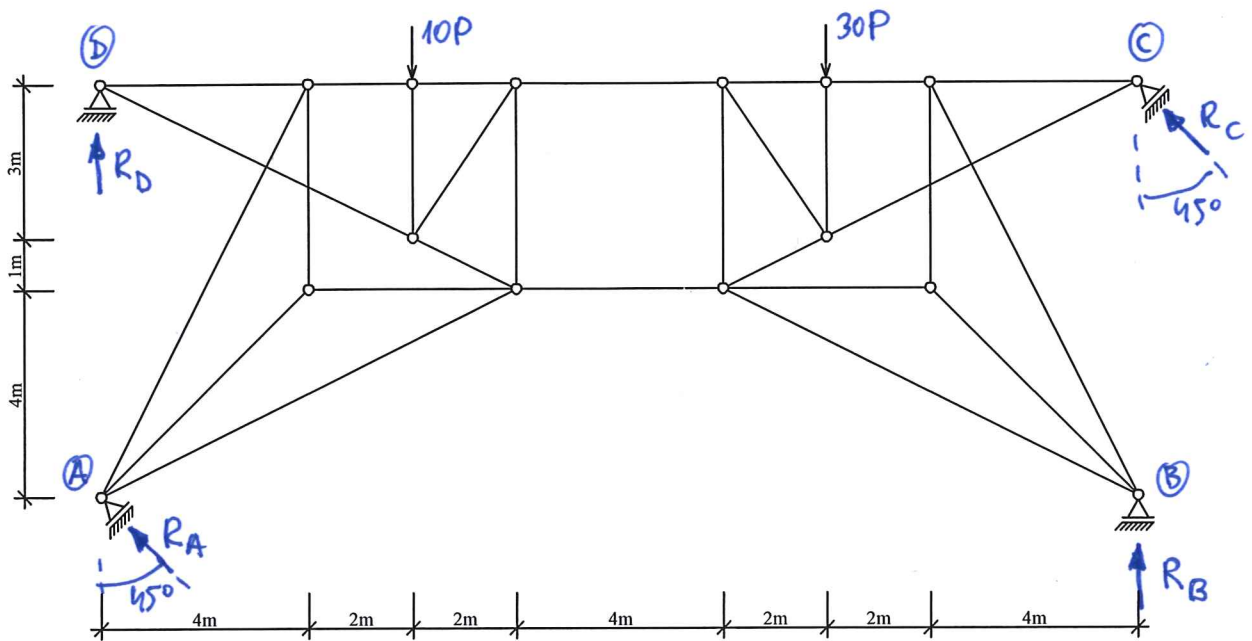
$|BB''| = 1$, $|EE''|_y = 1$, $|DD''|_x = \frac{6}{5}$
 $|EE''|_x = \frac{4}{5}$, $|CC''|_x = \frac{4}{5}$

$$-H \cdot |AA''| - \frac{9+6}{2} \cdot 2 \cdot |AA''| - \frac{1}{2} \cdot 6 \cdot 4 \cdot |BB''| + 30 \cdot |EE''|_x + 30 |EE''|_y +$$

$$- \frac{1}{2} \cdot 12 \cdot 4 \cdot \frac{1}{3} \cdot |CC''|_x = 0$$

$$-H - 15 - 12 + 30 \cdot \frac{4}{5} + 30 - 8 \cdot \frac{4}{5} = 0$$

$$H = 20,6 \text{ kN}$$



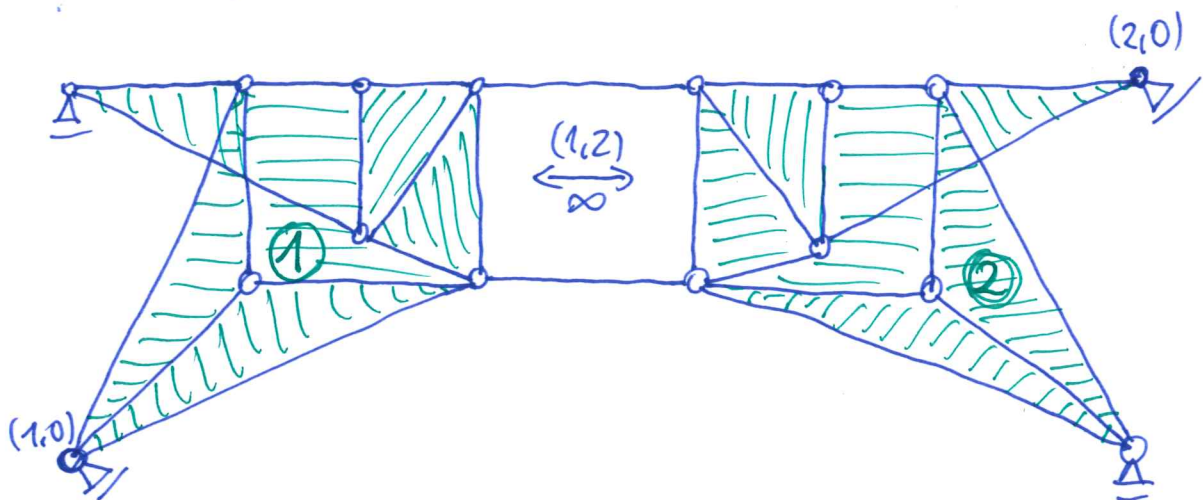
1. Sprawdzenie GN i SW

* warunki ilościowy

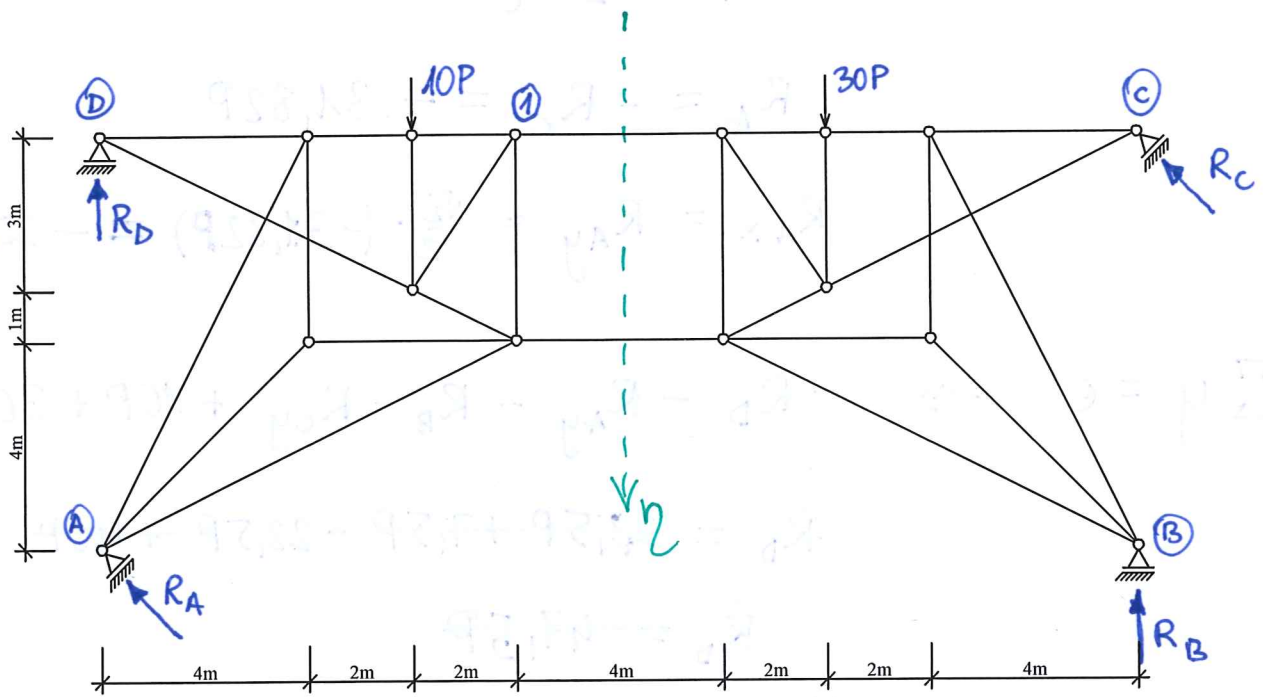
$$n = 2w - p - r$$

$$n = 2 \cdot 16 - 28 - 4 = 0$$

* warunki jakościowy



W postaci kinematycznej można wyodrębnić dwie tarcze, które tworzą 2 ostoję (tarcza 0) układ GN na mocy t.d. o 3 tarczach



2. Reakcije

$$\sum M_A = 0 \rightarrow -20 \cdot \frac{\sqrt{2}}{2} R_C - 8 \cdot \frac{\sqrt{2}}{2} R_C - 20 R_B + 6 \cdot 10P + 14 \cdot 30P = 0$$

War. konstruktivnyj $\sum \eta(p) = 0$

$$30P - \frac{\sqrt{2}}{2} R_C - R_B = 0$$

$$R_B = -\frac{\sqrt{2}}{2} R_C + 30P$$

Stpod:

$$-10\sqrt{2} R_C - 4\sqrt{2} R_C + 10\sqrt{2} R_C - 600P + 60P + 420P = 0$$

$$R_C = -21,213P$$

$$R_{Cx} = R_{Cy} = -\frac{\sqrt{2}}{2} \cdot 21,213P = -15P$$

$$R_B = +15P + 30P = 45P$$

$$\sum x = 0 \rightarrow -\frac{\sqrt{2}}{2} R_A - \frac{\sqrt{2}}{2} R_C = 0$$

$$R_A = -R_C = 21,213P$$

$$R_{Ax} = R_{Ay} = \frac{\sqrt{2}}{2} \cdot (21,213P) = 15P$$

$$\sum y = 0 \rightarrow -R_D - R_{Ay} - R_B - R_{Cy} + 10P + 30P = 0$$

$$R_D = -15P - 45P - (-15P) + 40P$$

$$R_D = -5P$$

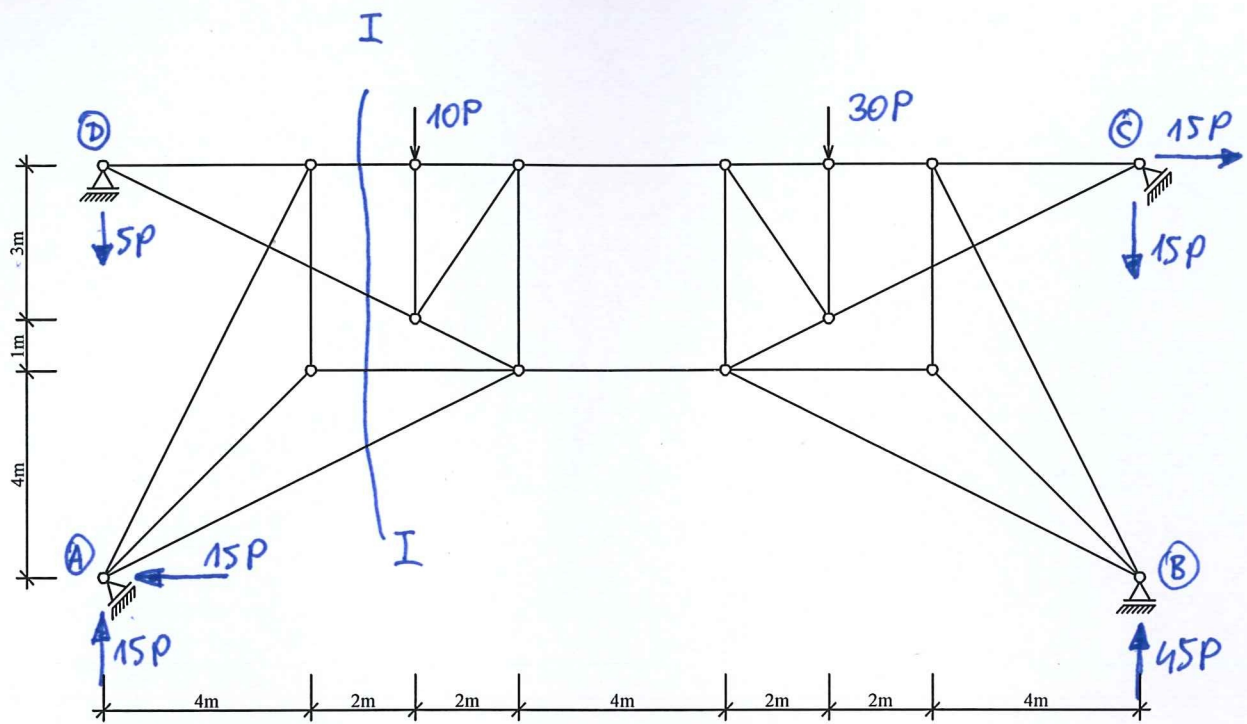
Sprawozdanie

$$\sum M_1 = 0$$

$$8R_{Ay} + 8R_{Ax} + 8R_D - 2 \cdot 10P + 6 \cdot 30P - 12R_{Cy} - 12R_B =$$

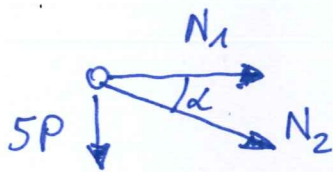
$$= 8 \cdot 15P + 8 \cdot 15P + 8 \cdot (-5P) - 20P + 180P - 12 \cdot (-15P) - 12 \cdot 45P =$$

$$= 600P - 600P = 0$$



3. Wymiarowanie sił w rozważonym przęśle

3.1. Równowaga węzła (D)



$$\cos \alpha = \frac{2}{\sqrt{5}}$$

$$\sin \alpha = \frac{1}{\sqrt{5}}$$

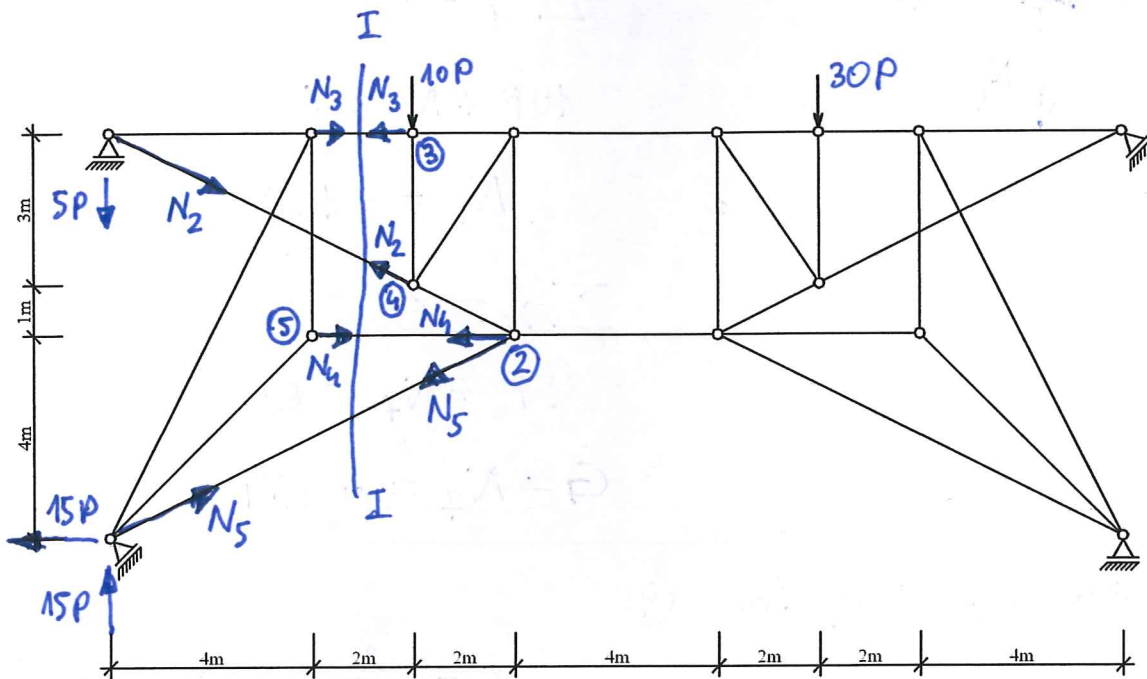
$$\sum y = 0 \quad 5P + \frac{1}{\sqrt{5}} N_2 = 0$$

$$N_2 = -5\sqrt{5}P$$

$$\sum x = 0 \quad N_1 + \frac{2}{\sqrt{5}} N_2 = 0$$

$$N_1 = -\frac{2}{\sqrt{5}} \cdot (-5\sqrt{5}P) = 10P$$

3.2. Pruefung Ritterschnitt I-I



$$\sum M_2(l) = 0 \quad 8 \cdot 15P + 4 \cdot 15P + 4 \cdot N_3 - 8 \cdot 5P = 0$$

$$N_3 = -35P$$

$$\sum y(l) = 0 \quad -15P + 5P + \frac{1}{\sqrt{5}}N_2 - \frac{1}{\sqrt{5}}N_5 = 0$$

$$-10P + \frac{1}{\sqrt{5}} \cdot (-5\sqrt{5}P) = \frac{1}{\sqrt{5}}N_5$$

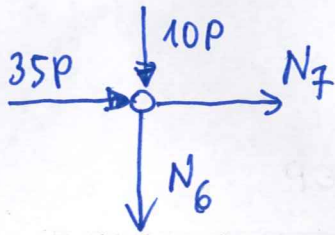
$$N_5 = -15\sqrt{5}P = -33,541P$$

$$\sum x(l) = 0 \quad -15P + \frac{2}{\sqrt{5}}N_5 + \frac{2}{\sqrt{5}}N_2 + N_3 + N_4 = 0$$

$$-15P + \frac{2}{\sqrt{5}} \cdot (-15\sqrt{5}P) + \frac{2}{\sqrt{5}} \cdot (-5\sqrt{5}) - 35P + N_4 = 0$$

$$N_4 = 90P$$

3.3. Równowaga węzła (3)



$$\sum y = 0$$

$$10P + N_6 = 0$$

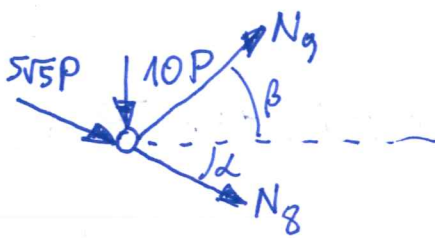
$$N_6 = -10P$$

$$\sum x = 0$$

$$35P + N_7 = 0$$

$$N_7 = -35P$$

3.4. Równowaga węzła (4)



$$\cos \beta = \frac{2}{\sqrt{13}}, \quad \sin \beta = \frac{3}{\sqrt{13}}$$

$$\sum x = 0$$

$$5\sqrt{5}P \cdot \frac{2}{\sqrt{5}} + \frac{2}{\sqrt{5}}N_8 + \frac{2}{\sqrt{13}}N_9 = 0$$

$$\sum y = 0$$

$$-\frac{3}{\sqrt{13}}N_9 + \frac{1}{\sqrt{5}}N_8 + 10P + \frac{1}{\sqrt{5}} \cdot 5\sqrt{5}P = 0$$

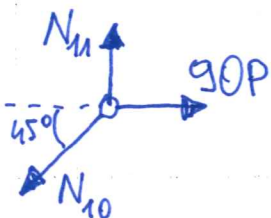
$$N_9 = \frac{\sqrt{13}}{3\sqrt{5}}N_8 + \frac{15\sqrt{13}}{3}P$$

$$0 = 10P + \frac{2}{\sqrt{5}}N_8 + \frac{2}{\sqrt{13}} \cdot \frac{\sqrt{13}}{3\sqrt{5}}N_8 + \frac{2}{\sqrt{13}} \cdot \frac{15\sqrt{13}}{3}P$$

$$1,1926N_8 = -20P$$

$$N = N_8 = -16,77P$$

3.5. Równowaga węzła (5)

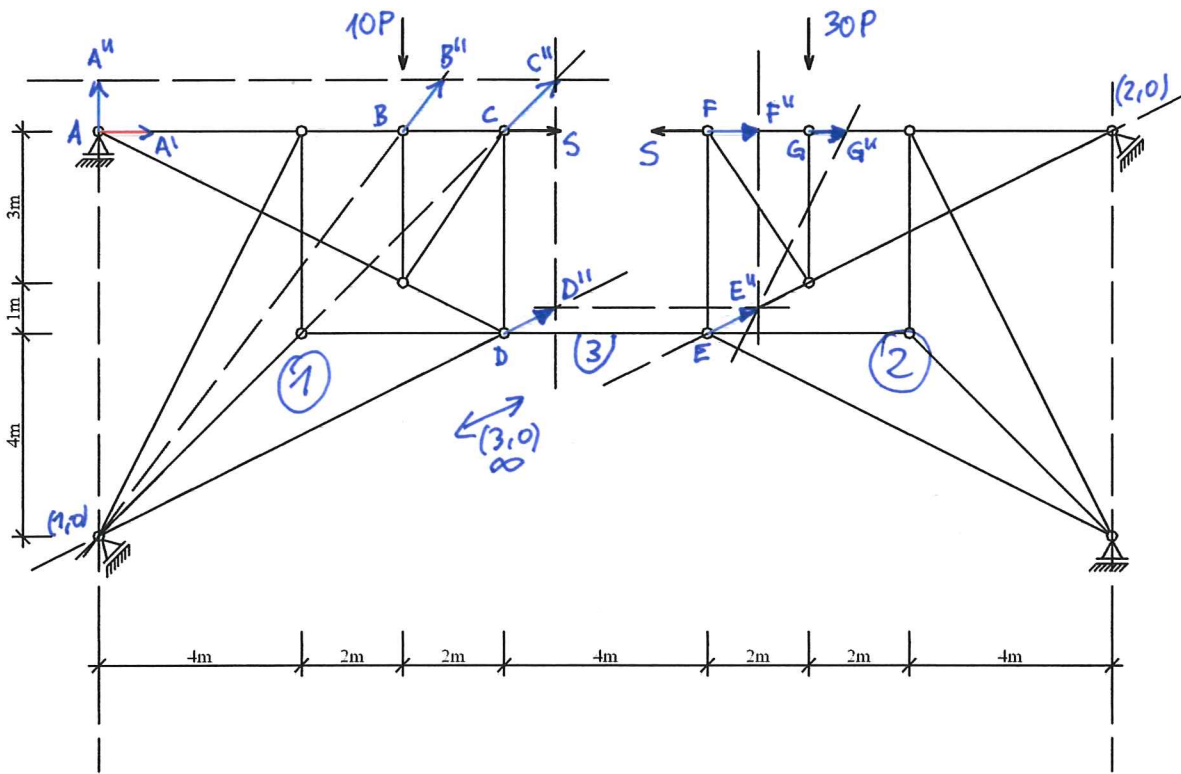


$$\sum x = 0$$

$$-\frac{\sqrt{2}}{2} \cdot N_{10} + 90P = 0$$

$$K = N_{10} = +127,279P$$

Medanimum u S^u



$$|AA^u| = 1 - \text{penn medane}$$

$$|BB^u|_x = \frac{3}{4}$$

$$|CC^u|_y = 1, |CC^u|_x = 1$$

$$|DD^u|_x = 1, |DD^u|_y = \frac{1}{2}$$

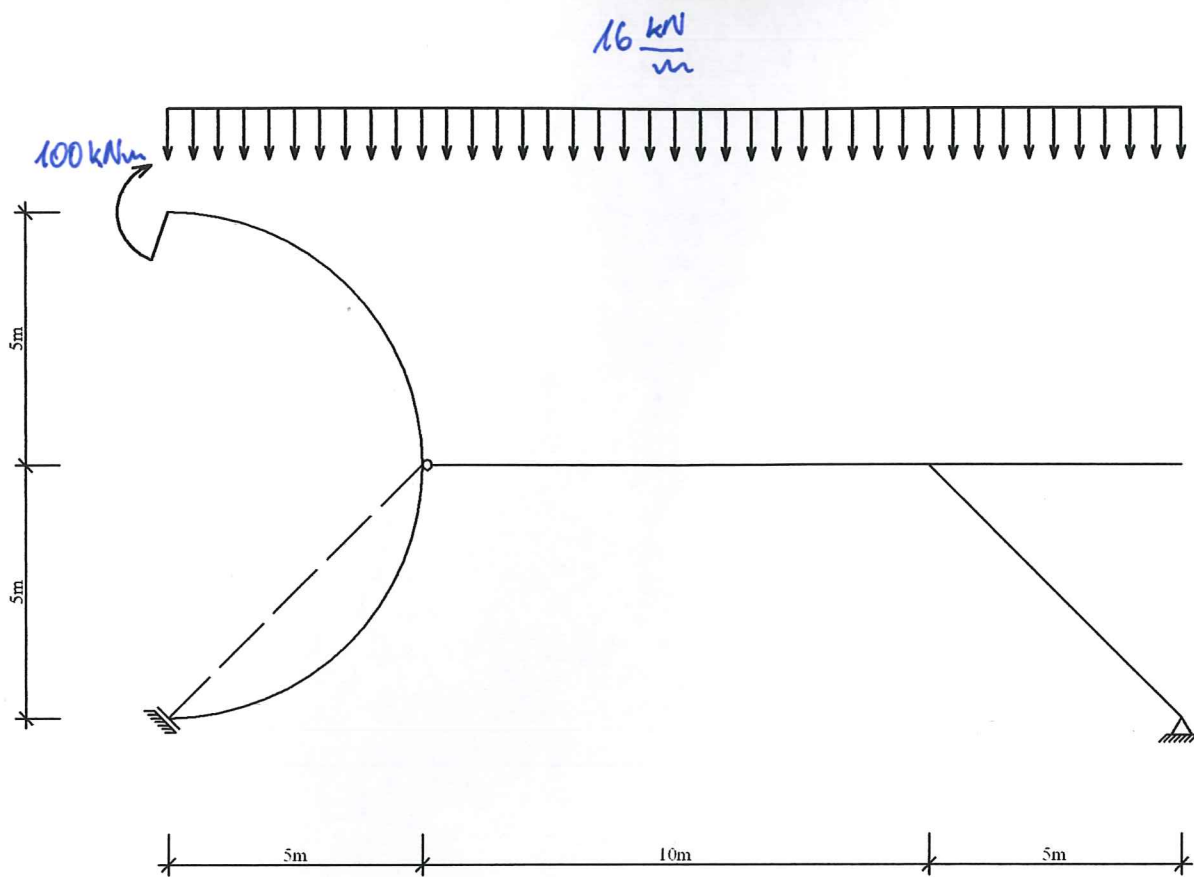
$$|EE^u|_x = 1, |EE^u|_y = \frac{1}{2}$$

$$|FF^u| = 1, |GG^u| = \frac{3}{4}$$

$$L = -10P \cdot |BB^u|_x - S \cdot |CC^u|_y - 30P \cdot |GG^u| = 0$$

$$-10P \cdot \frac{3}{4} - S - 30P \cdot \frac{3}{4} = 0$$

$$S = -30P$$



1 Sprawdzenie GN i SW

* warunki ilościowy

$$n = e - 3t$$

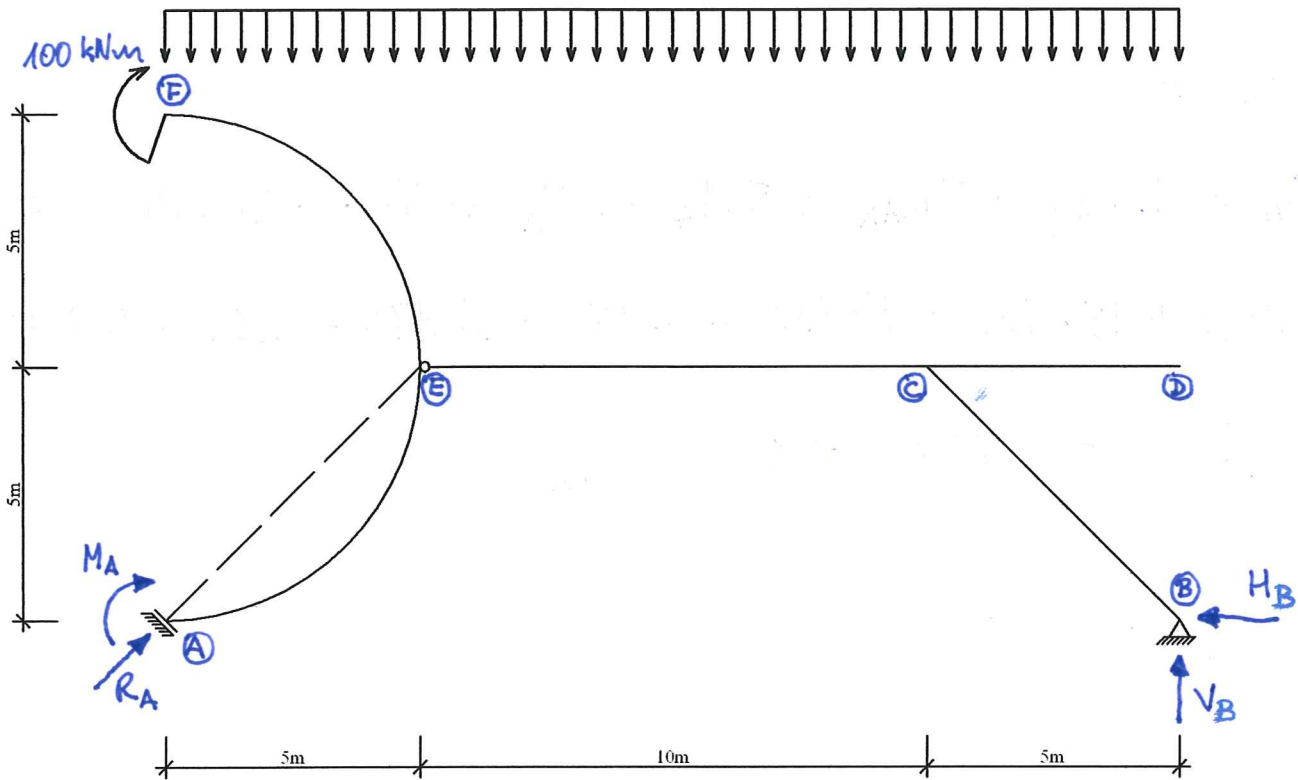
$$n = 6 - 3 \cdot 2 = 0$$

* warunki jakościowy

Na mocy twierdzenia o 3 torach uśrednia się geometryczną nieciągłość układu.

Razem jest GN i SW ($n=0$).

$$16 \frac{\text{kN}}{\text{m}}$$



2. Reakije

Wormmel konstantkijung: $\sum M_E(l) = 0$

$$M_A + 100 - 16 \cdot 5 \cdot 2,5 = 0$$

$$M_A = 100 \text{ kNm}$$

$$\sum M_A = 0 \rightarrow -20V_B + 20 \cdot 16 \cdot 10 + 100 + 100 = 0$$

$$V_B = 170 \text{ kN}$$

$$\sum y = 0 \rightarrow -\frac{\sqrt{2}}{2} R_A + 16 \cdot 20 - V_B = 0$$

$$R_A = 212,132 \text{ kN}$$

$$R_{Ax} = R_{Ay} = 150 \text{ kN}$$

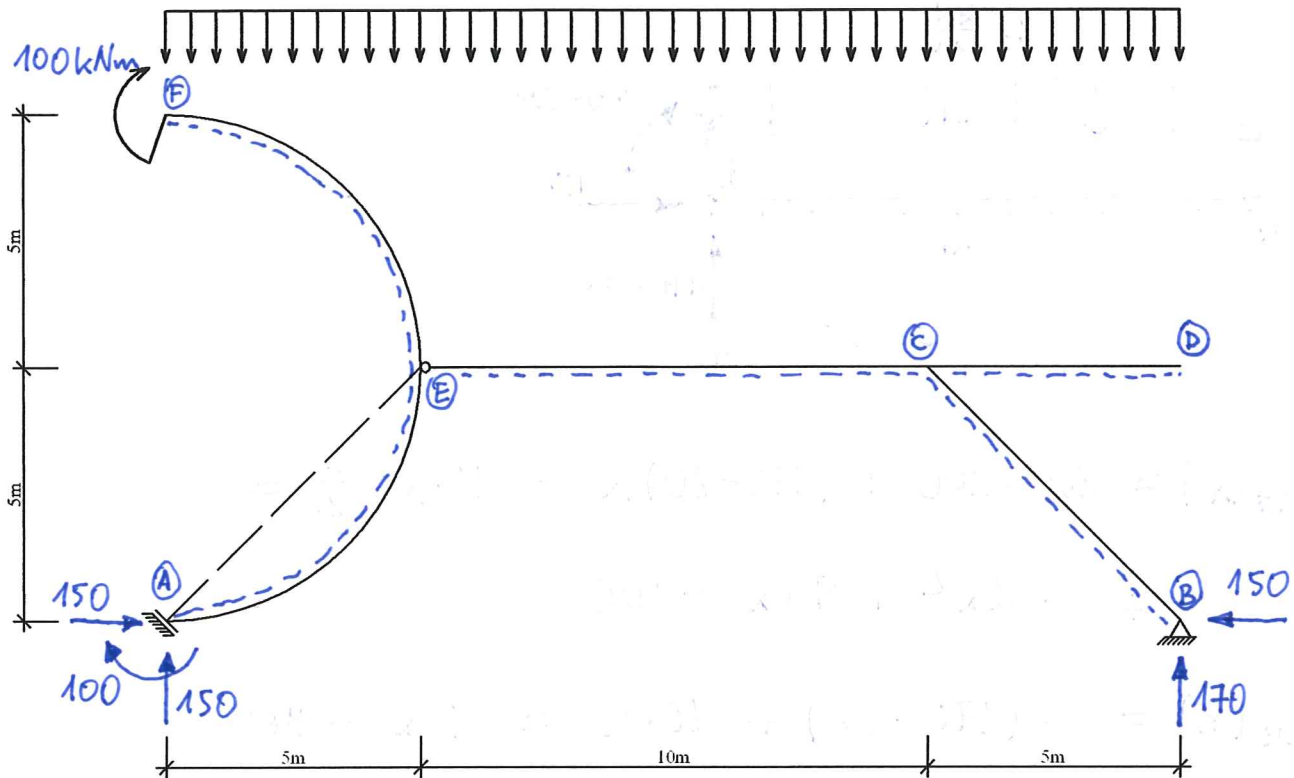
$$\sum x = 0 \rightarrow R_{Ax} - H_B = 0 \rightarrow H_B = 150 \text{ kN}$$

Sprawdzenie :

$$\sum M_c = 0$$

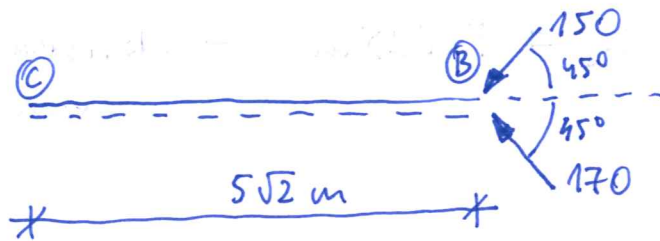
$$\begin{aligned} M_A + 15R_{Ay} - 5R_{Ax} + 5H_A - 5V_A - 5 \cdot 20 \cdot 16 + 100 &= \\ = 100 + 15 \cdot 150 - 5 \cdot 150 + 5 \cdot 150 - 5 \cdot 170 - 1600 + 100 &= \\ = 3200 - 3200 = 0 &\quad \text{ok} \end{aligned}$$

$$16 \frac{\text{kN}}{\text{m}}$$



3. siły przekrojowe

3.1. Przedział B-C



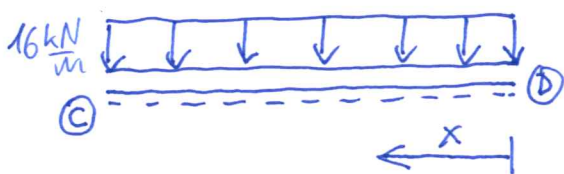
$$M_{BC} = 0$$

$$M_{CB} = \frac{\sqrt{2}}{2} \cdot 170 \cdot 5\sqrt{2} - \frac{\sqrt{2}}{2} \cdot 150 \cdot 5\sqrt{2} = 100 \text{ kNm}$$

$$T_{BC} = T_{CB} = \frac{\sqrt{2}}{2} \cdot 150 - \frac{\sqrt{2}}{2} \cdot 170 = -14,142 \text{ kN}$$

$$N_{BC} = N_{CB} = -\frac{\sqrt{2}}{2} \cdot 150 - \frac{\sqrt{2}}{2} \cdot 170 = -226,274 \text{ kN}$$

3.2. Przedział D-C ($0 \leq x \leq 5\text{m}$)



$$M_{DC}(x) = -16 \cdot x \cdot \frac{x}{2} = -8x^2$$

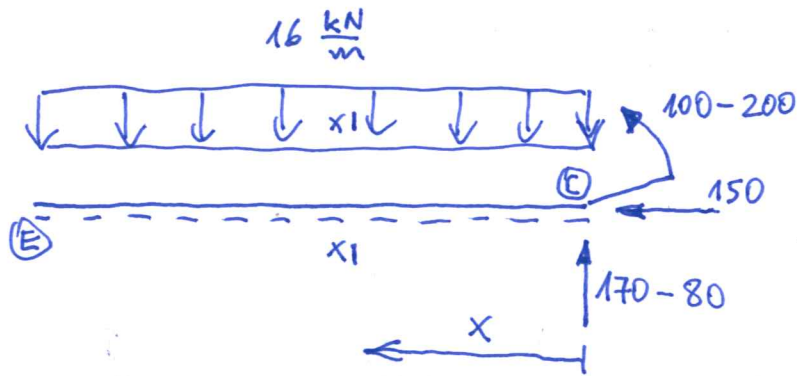
$$T_{DC}(x) = 16 \cdot x$$

$$N_{DC}(x) \equiv 0$$

$$M_{DC}(0) = 0, M_{DC}(2,5\text{m}) = -50 \text{ kNm}, M_{DC}(5\text{m}) = -200 \text{ kNm}$$

$$T_{DC}(0) = 0, T_{DC}(2,5\text{m}) = 40 \text{ kN}, T_{DC}(5\text{m}) = 80 \text{ kN}$$

3.3. Predikat C-E ($0 \leq x \leq 10\text{m}$)



$$M_{CE}(x) = 100 - 200 + (170 - 80)x - 16 \cdot x \cdot \frac{x}{2} =$$

$$= -8x^2 + 90x - 100$$

$$T_{CE}(x) = -(170 - 80) + 16 \cdot x = 16x - 90$$

$$N_{CE}(x) = -150$$

$$T_{CE}(x_0) = 0 \Leftrightarrow 16x - 90 = 0$$

$$x_0 = 5,625\text{m} \quad - \text{ekstremum momentu}$$

$$M_{CE}(0) = -100 \text{ kNm}$$

$$M_{CE}(5,625\text{m}) = M_{CE}^{\max} = 153,125 \text{ kNm}$$

$$M_{CE}(10\text{m}) = 0 \quad - \text{w podporcie}$$

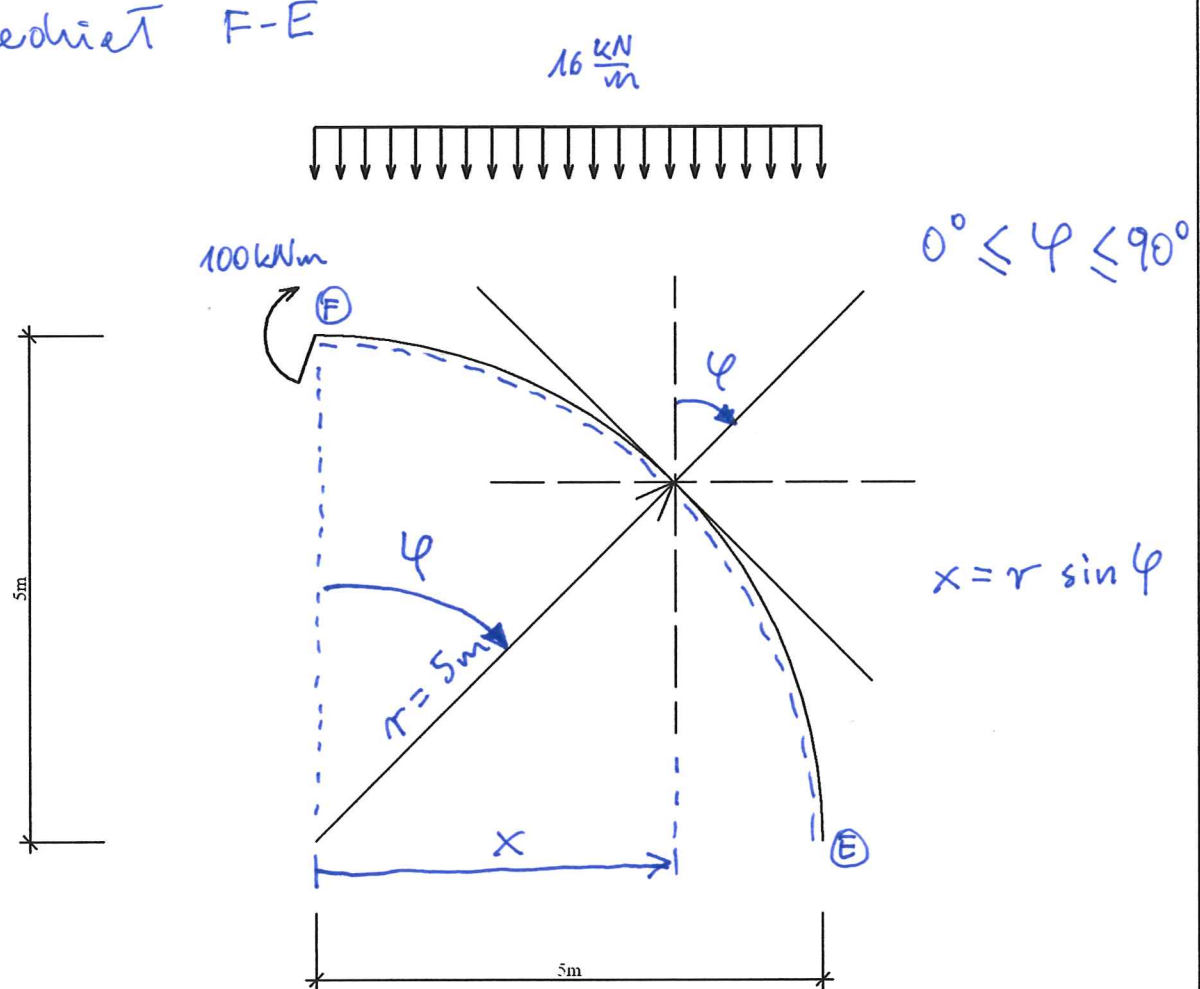
$$T_{CE}(0) = -90 \text{ kN}$$

$$T_{CE}(10\text{m}) = 70 \text{ kN}$$

$$N_{CE}(0) = -150 \text{ kN}$$

$$N_{CE}(10\text{m}) = -150 \text{ kN}$$

3.4. Prediét F-E



$$M_{FE}(\varphi) = 100 - 16 \cdot x \cdot \frac{x}{2} = 100 - 8 \cdot 5^2 \cdot \sin^2 \varphi =$$

$$= -200 \sin^2 \varphi + 100$$

$$T_{FE}(\varphi) = -16 \cdot x \cdot \cos \varphi = -16 \cdot 5 \cdot \sin \varphi \cdot \cos \varphi =$$

$$= -80 \sin \varphi \cdot \cos \varphi$$

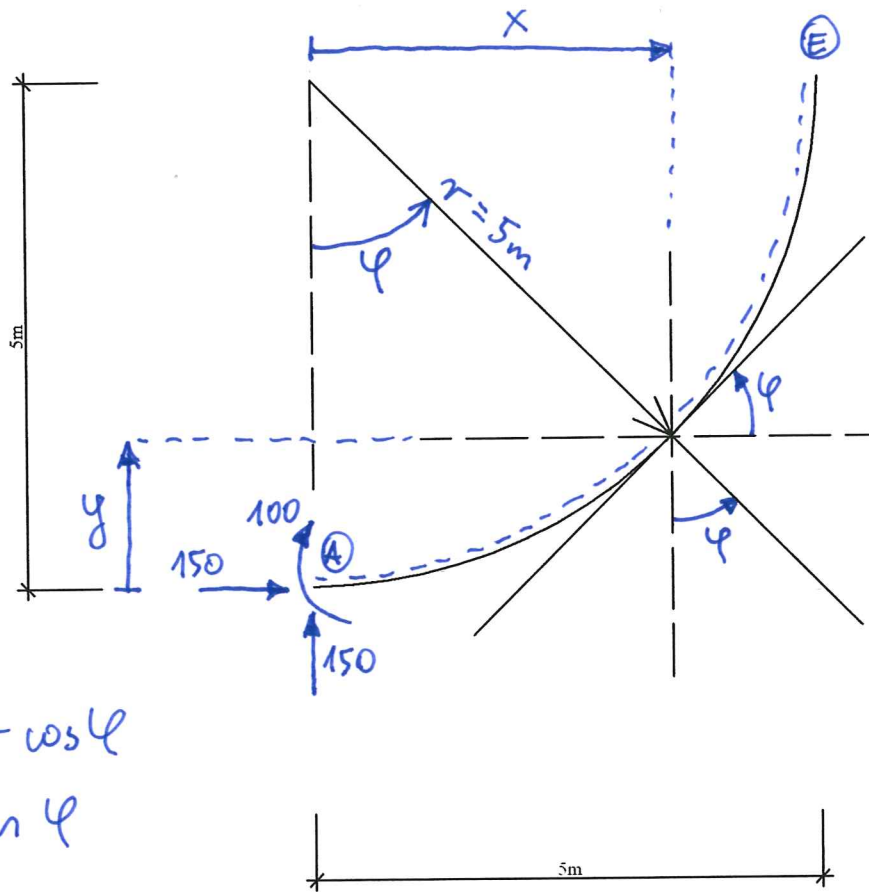
$$N_{FE}(\varphi) = -16 \cdot x \cdot \sin \varphi = -16 \cdot 5 \cdot \sin \varphi \cdot \sin \varphi =$$

$$= -80 \sin^2 \varphi$$

φ [deg]	$M(\varphi)$ [kNm]	$T(\varphi)$ [kN]	$N(\varphi)$ [kN]
0	100,000	0,000	0,000
15	86,603	-20,000	-5,359
30	50,000	-34,641	-20,000
45	0,000	-40,000	-40,000
60	-50,000	-34,641	-60,000
75	-86,603	-20,000	-74,641
90	-100,000	0,000	-80,000

3.5. Pseudiat A-E

$$0^\circ \leq \varphi \leq 90^\circ$$



$$y = r - r \cos \varphi$$

$$x = r \sin \varphi$$

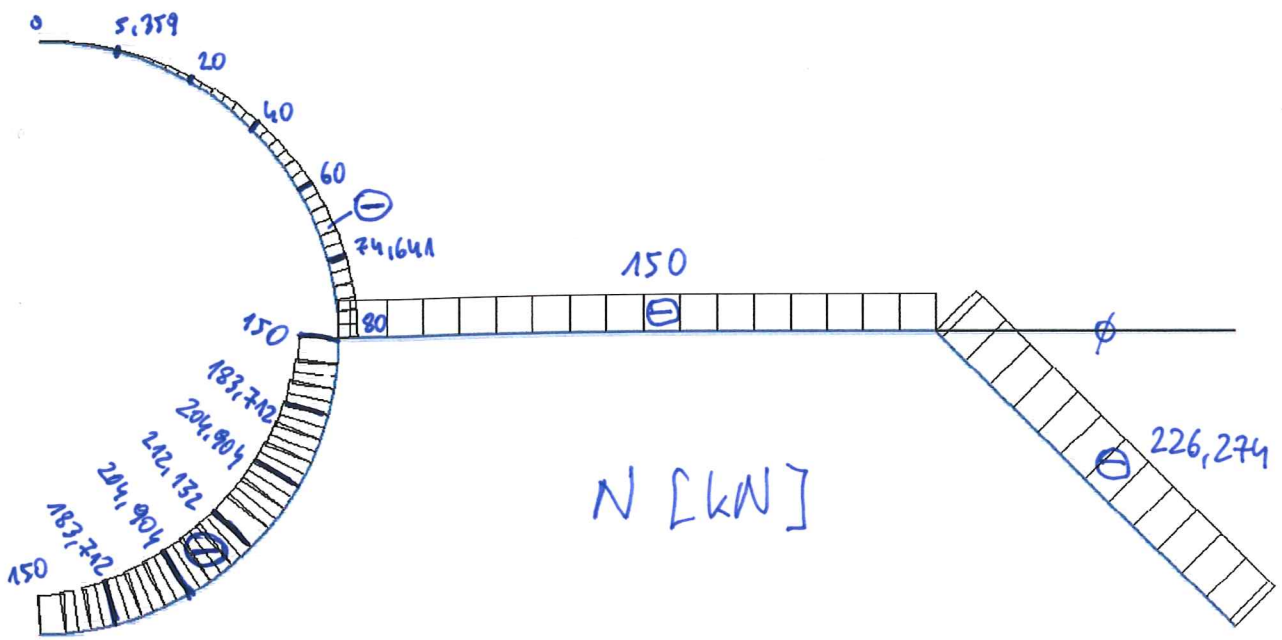
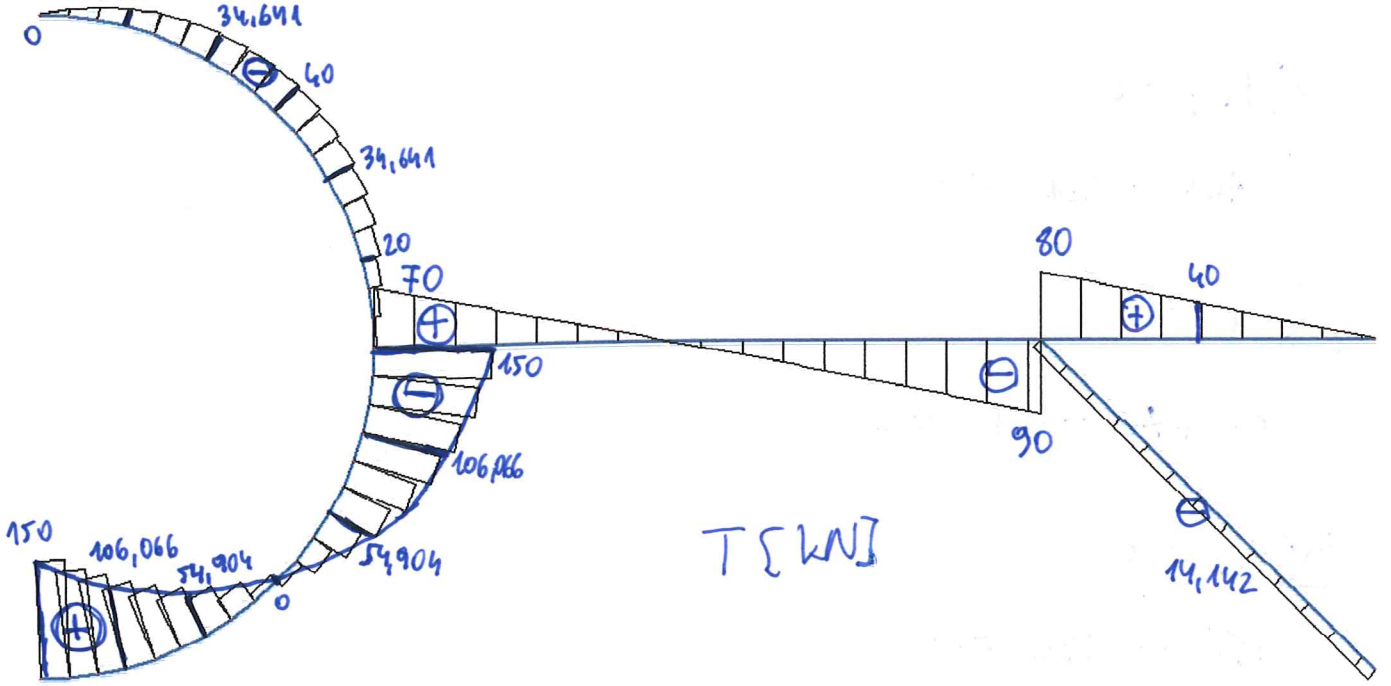
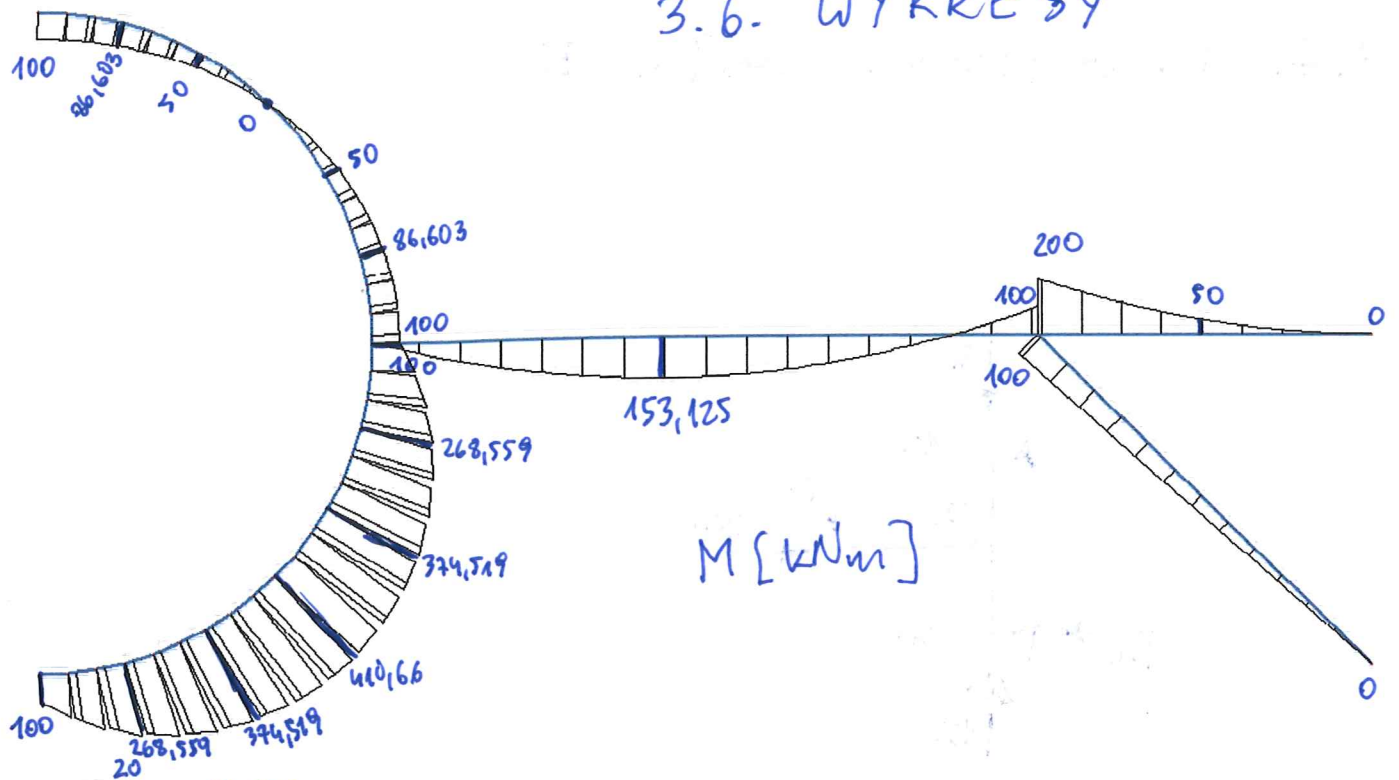
$$\begin{aligned} M_{AE}(\varphi) &= -100 - 150x + 150y = \\ &= -100 - 150 \cdot 5 \cdot \sin \varphi + 150(5 - 5 \cos \varphi) = \\ &= 650 - 750 \sin \varphi - 750 \cos \varphi \end{aligned}$$

$$T_{AE}(\varphi) = 150 \cos \varphi - 150 \sin \varphi$$

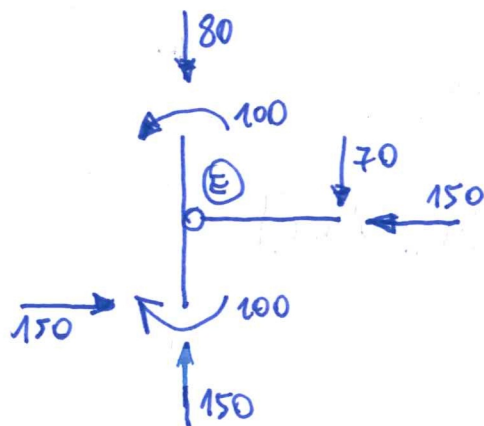
$$N_{AE}(\varphi) = -150 \cos \varphi - 150 \sin \varphi$$

φ [deg]	$M(\varphi)$ [kNm]	$T(\varphi)$ [kN]	$N(\varphi)$ [kN]
0	-100,000	150,000	-150,000
15	-268,559	106,066	-183,712
30	-374,519	54,904	-204,904
45	-410,660	0,000	-212,132
60	-374,519	-54,904	-204,904
75	-268,559	-106,066	-183,712
90	-100,000	-150,000	-150,000

3.6. WYKRESY



3.7. Równowaga węzła (E)



$$\sum M_E = 0$$

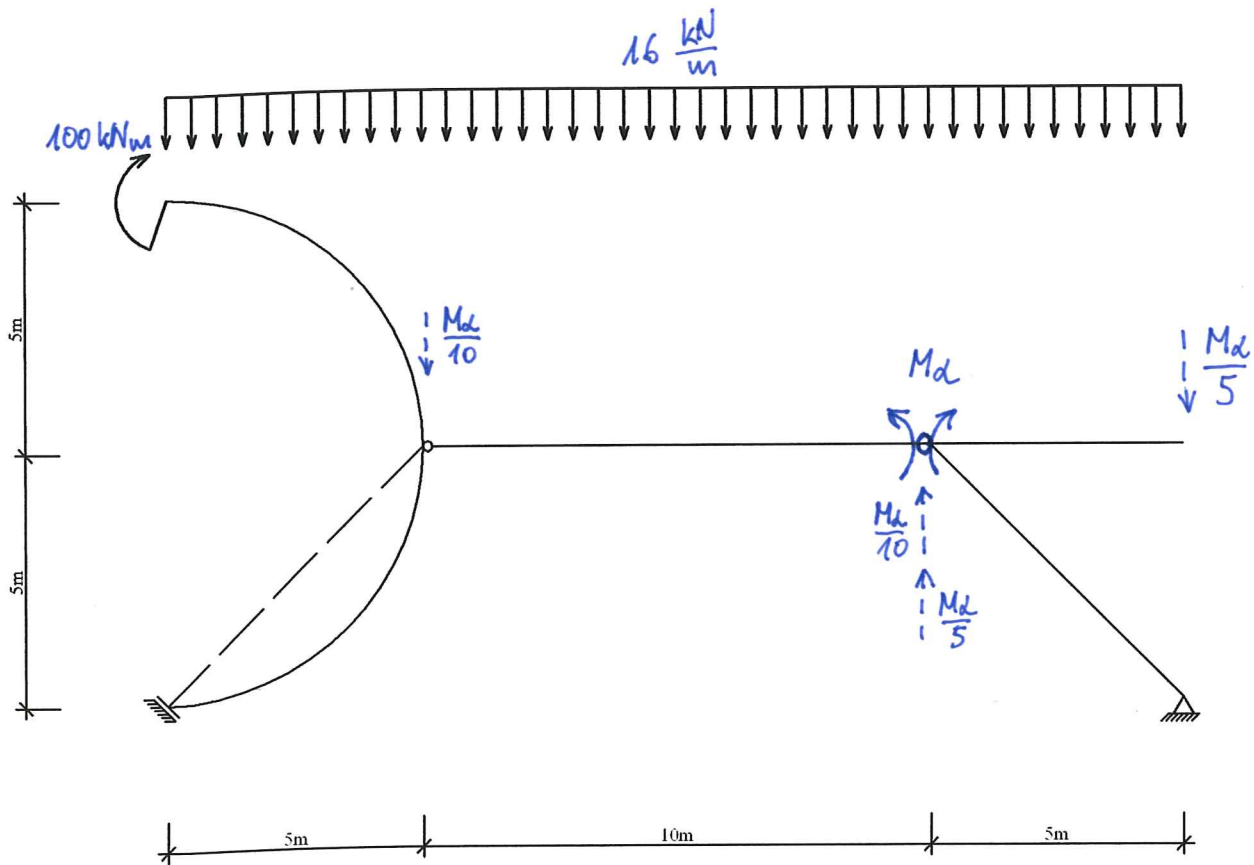
$$100 - 100 = 0$$

$$\sum y = 0$$

$$80 + 70 - 150 = 0$$

$$\sum x = 0$$

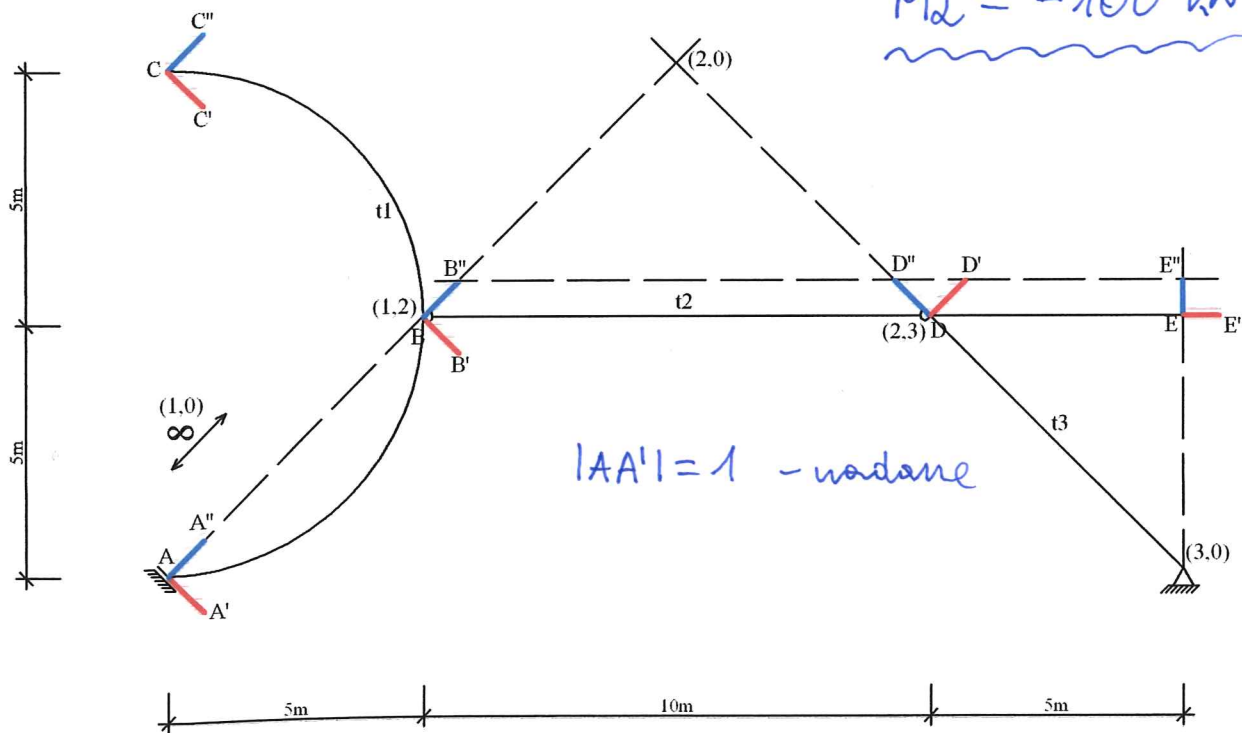
$$150 - 150 = 0$$



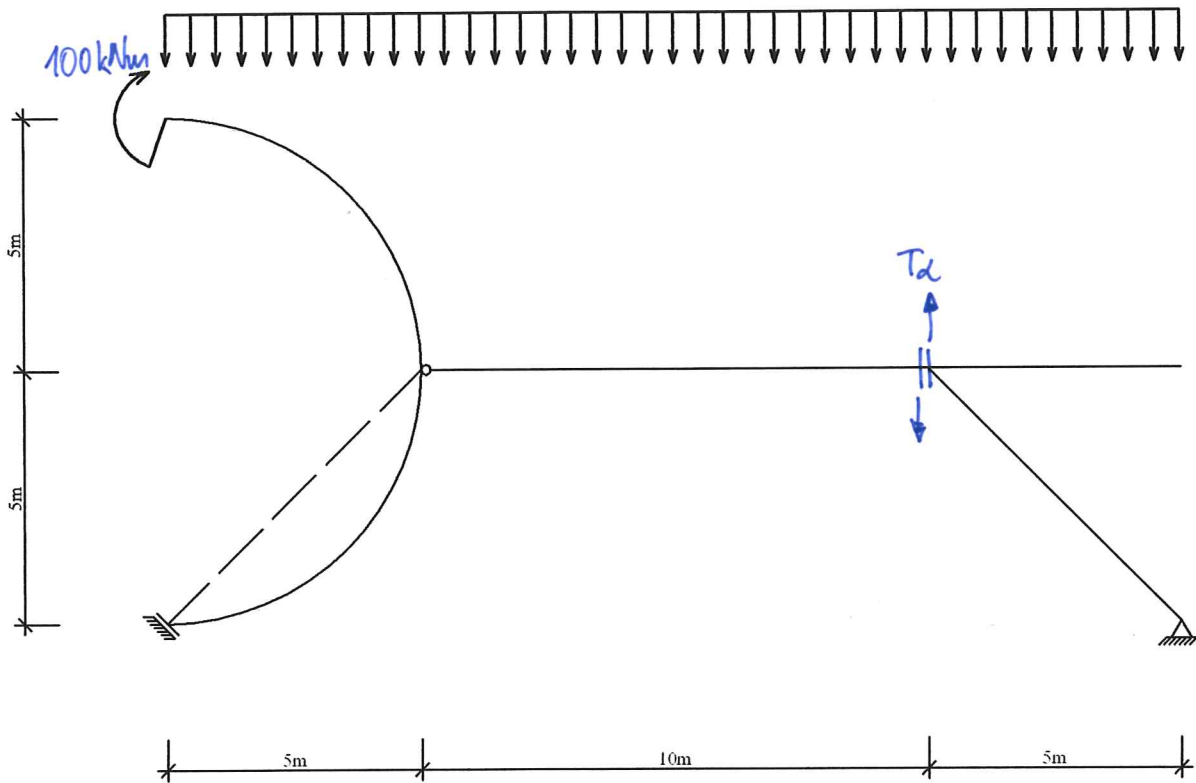
Mechanism M_d

$$L = -16 \cdot 5 \cdot \frac{\sqrt{2}}{2} \cdot 1 - 16 \cdot \frac{10}{2} \cdot \frac{\sqrt{2}}{2} \cdot 1 + 16 \cdot \frac{10}{2} \cdot \frac{\sqrt{2}}{2} \cdot 1 + 16 \cdot \frac{5}{2} \cdot \frac{\sqrt{2}}{2} \cdot 1 - \frac{M_d}{10} \cdot \frac{\sqrt{2}}{2} \cdot 1 - \frac{M_d}{10} \cdot \frac{\sqrt{2}}{2} \cdot 1 - \frac{M_d}{5} \cdot \frac{\sqrt{2}}{2} \cdot 1 = 0$$

$M_d = -100 \text{ kNm}$



16 $\frac{kN}{m}$

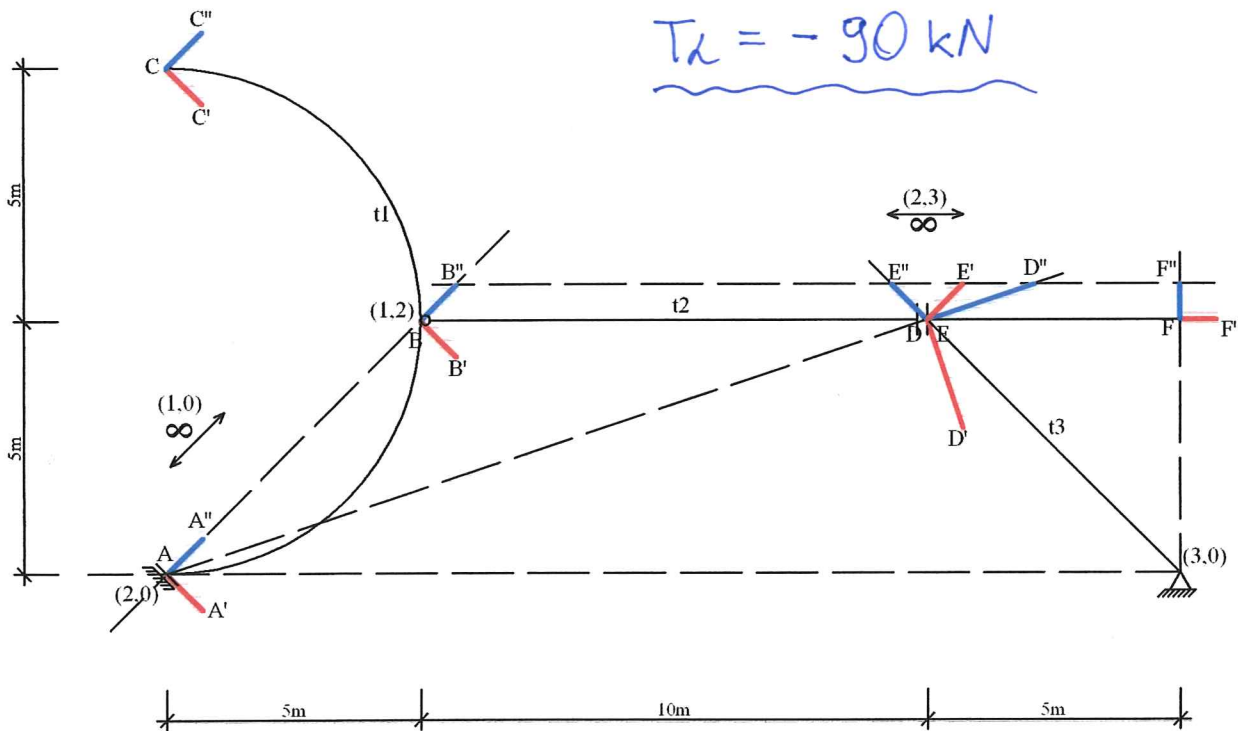


MECHANIZM T_d

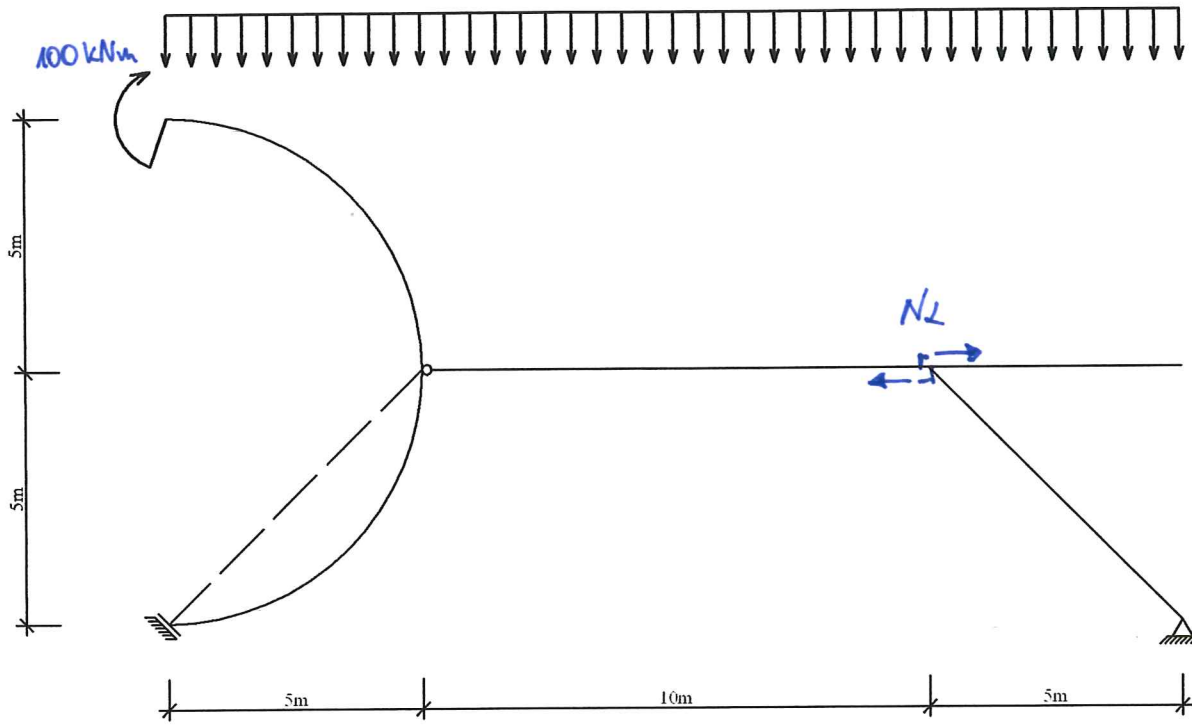
$|AA'| = 1$ - wadane

$$L = -16 \cdot 5 \cdot \frac{\sqrt{2}}{2} \cdot 1 - 16 \cdot \frac{10}{2} \cdot \frac{\sqrt{2}}{2} \cdot 1 - 16 \cdot \frac{10}{2} \cdot \frac{\sqrt{2}}{2} \cdot 3 + 16 \cdot \frac{5}{2} \cdot \frac{\sqrt{2}}{2} \cdot 1 - T_d \cdot \frac{\sqrt{2}}{2} \cdot 3 - T_d \cdot \frac{\sqrt{2}}{2} \cdot 1 = 0$$

$T_d = -90 \text{ kN}$



16 $\frac{kN}{m}$



MECHANIZM N_d

$|AA'| = 1$ wadane

$$L = -16 \cdot 5 \cdot \frac{\sqrt{2}}{2} \cdot 1 - 16 \cdot 10 : 2 \cdot \frac{\sqrt{2}}{2} \cdot 1 - 16 \cdot 10 : 2 \cdot \frac{\sqrt{2}}{2} \cdot \frac{1}{3} - 16 \cdot 5 : 2 \cdot \frac{\sqrt{2}}{2} \cdot \frac{1}{3} - N_d \cdot \frac{\sqrt{2}}{2} \cdot 1 - N_d \cdot \frac{\sqrt{2}}{2} \cdot \frac{1}{3} = 0$$

$N_d = -150 \text{ kN}$

